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SPECIFICATION

TITLE OF THE INVENTION

CUT OFF METHOD AND APPARATUS FOR BAND-LIKE PAPER

5 AND CONTROL APPARATUS FOR THE SAME

FIELD OF THE INVENTION

[0001]

10 The present invention relates to a cut off method
and apparatus for band-like paper, such as a corrugated
fiberboard web, and a control apparatus for the same in
a corrugating machine which manufactures corrugated
fiberboard sheets, etc.

15 BACKGROUND OF THE INVENTION

[0002]

20 In a previous cut off apparatus in a corrugating
machine, various attempts have been made to reduce the
rigidity of knife cylinders and to realize a specified
pressing force between knives. In FIG. 8, for example,
the cut off apparatus includes: an upper knife cylinder
53 to which an upper knife 55 and split gears 8a and 8b
are attached; a lower knife cylinder 54 to which a lower
knife 56, which cuts a corrugated fiberboard web in
25 cooperation with the upper knife 55, and a lower gear 9
which has a meshing engagement with the split gears 8a
and 8b are attached; a main drive motor 51 and an auxiliary

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drive motor 50 which rotationally drive the knife cylinders 53 and 54; and a controller 52 which controls the drive motors 51 and 50. Clearance is formed between the teeth of the split gears 8a and 8b and the teeth of the lower gear 9, which teeth have a meshing engagement with one another when the upper and lower knives 55 and 56 come into contact with each other. The controller 52 controls at least either one of the drive motors 51 and 50 so that a pressing force is applied between the knives 55 and 56 when these knives come into contact with each other (for example, the following patent document 1).

[Patent document 1] Japanese Patent Application Laid-open No. 2002-284430

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DISCLOSURE OF THE INVENTION

PROBLEMS TO BE SOLVED BY THE INVENTION

[0003]

However, the controller 52 in the above patent document 1 only performs torque control in such a manner that a pressing force is generated so that the upper knife 55 is pressed against the lower knife 56. Thus, it is difficult to accurately cut off band-like paper such as a corrugated fiberboard sheet. Further, the rated power capacities (size) of the upper motor and the lower motor are different, so that the number of types of components including a control device is increased.

[0004]

With the foregoing problems in view, it is an object of the present invention to provide a cut off method and apparatus for band-like paper and a control apparatus for the same, in which torque necessary for cutting off the band-like paper is properly distributed to the upper (preceding) and the lower (following) motor, so that the band-like paper such as a corrugated fiberboard sheet is accurately cut off. Further it is another object of the present invention to reduce the number of types of components by equalizing the rated power capacities of the upper motor and the lower motor.

MEANS TO SOLVE THE PROBLEMS

[0005]

15 In order to accomplish the above object, according to the present invention, a cut off method for a cut off apparatus as set forth in claim 1 is characterized in that which apparatus includes: a preceding knife cylinder on whose peripheral surface a preceding helical knife is provided; a following knife cylinder on whose peripheral surface a following helical knife, which cuts off band-like paper in cooperation with the preceding knife, is provided; a preceding knife driving motor which rotationally drives the preceding knife cylinder; a following knife driving motor which rotationally drives the following knife cylinder; and a cut off control device which individually controls the preceding knife driving

motor and the following knife driving motor, wherein the method comprises: giving, when the band-like paper is cut, the preceding knife and the following knife a specified amount of torque in the direction in which the preceding
5 knife and the following knife are pressed against each other, by means of the preceding knife driving motor and the following knife driving motor.

[0006]

A cut off method as set forth in claim 2 is
10 characterized in that the value of the torque given by means of the preceding knife driving motor is the same as the value of the torque given by means of the following knife driving motor.

A cut off control device for band-like paper as set
15 forth in claim 3, which device controls a preceding knife driving motor for rotationally driving a preceding knife cylinder on whose peripheral surface a preceding helical knife is provided and also a following knife driving motor for rotationally driving a following knife cylinder on
20 whose peripheral surface a following helical knife is provided, is characterized in that the device comprises: a speed pattern generator, to which a paper feeding speed of the band-like paper and the sheet length to be cut off is input, for generating rotational speed patterns of the
25 preceding knife driving motor and the following knife driving motor based on the input paper feeding speed and the input sheet length to be cut off and for outputting

a speed instruction value; a comparator which compares the speed instruction value from the speed pattern generator with a detected speed of the preceding knife driving motor or the following knife driving motor; an instruction torque computing unit which computes rotational torque instruction values for the preceding knife driving motor and the following knife driving motor based on a signal from the comparator; a cutting torque computing unit which computes cutting torque of the preceding knife driving motor and the following knife driving motor; a to-be-given torque pattern generator which distributes the cutting torque sent from the cutting torque computing unit, and generates a to-be-given torque pattern based on the paper feeding speed of the band-like paper and the sheet length to be cut off, and outputs a to-be-given torque instruction value; an instruction torque subtractor unit which subtracts the to-be-given torque instruction value, output from the to-be-given torque pattern generator, from the rotational torque instruction value computed by the instruction torque computing unit; a preceding power amplifier which controls the preceding knife driving motor based on a computation result obtained by the instruction torque subtractor; an instruction torque adder which adds the rotational torque instruction value, computed by the instruction torque computing unit, to the to-be-given torque instruction value computed by the to-be-given torque pattern

generator; and a following power amplifier which controls the following knife driving motor based on a computation result obtained by the instruction torque adder.

[0007]

5 A cut off control device as set forth in claim 4 is characterized in that, in the device as set forth in claim 3, the cutting torque computed by the cutting torque computing unit has a cutting torque value necessary for cutting off the band-like paper, the cutting torque value
10 being based on the basis weight and the paper feeding speed input.

 A cut off control device as set forth in claim 5 is characterized in that, in the device as set forth in claim 3 or claim 4, the cutting torque computed by the
15 cutting torque computing unit is large enough to resist a cut-off reactive force added from the band-like paper to the preceding and following knives, and also to give an appropriate contact force to the preceding and following knives.

20 [0008]

 A cut off control device as set forth in claim 6 is characterized in that, in the device as set forth in any one of claim 3 through claim 5, the to-be-given torque pattern generated by the to-be-given torque pattern
25 generator is a pattern having a rectangular shape, a trapezoidal shape, or a polygonal shape.

— ——— A cut off control device as set forth in claim 7

is characterized in that, in the device as set forth in any one of claim 3 through claim 6, the to-be-given torque pattern generator changes the pattern of the to-be-given torque depending on the paper feeding speed.

5 [0009]

A cut off control device as set forth in claim 8 is characterized in that, in the device as set forth in any one of claim 3 through claim 7, the to-be-given torque pattern generator generates an identical to-be-given torque pattern for the preceding knife driving motor and the following knife driving motor.

A cut off control device as set forth in claim 9 is characterized in that, in the device as set forth in any one of claim 3 through claim 8, the cut off control device is connected to a production management device including an input unit for inputting thereto the basis weight of the band-like paper and the sheet length to be cut off, which production management system (i) outputs the basis weight of the band-like paper to the cutting torque computing unit, and (ii) computes the rotation speeds of the preceding and following knife cylinders based on the basis weight of the band-like paper and the sheet length to be cut off, and (iii) outputs the resultant obtained rotation speed to the speed pattern generator.

25 [0010]

A cut off apparatus for cutting off band-like paper is characterized in that the apparatus comprises: a

preceding knife cylinder on whose peripheral surface a preceding helical knife is provided; a following knife cylinder on whose peripheral surface a following helical knife, which cuts off band-like paper in cooperation with the preceding knife, is provided; a preceding gear attached at one of the opposite ends of the rotation axis of the preceding knife cylinder; a following gear attached at one of the opposite ends of the rotation axis of the following knife cylinder; a preceding drive gear which has a meshing engagement with the preceding gear; a following drive gear which has a meshing engagement with the following gear; a preceding knife driving motor which rotationally drives the preceding drive gear; a following knife driving motor which rotationally drives the following drive gear, the following knife driving motor having the same rated capacity as that of the preceding knife driving motor; and a cut off control device which individually controls the preceding knife driving motor and the following drive gear.

[0011]

A cut off apparatus as set forth in claim 11 is characterized in that, in the apparatus as set forth in claim 10, at least either one of the preceding gear and the following gear has one or more teeth shaped so that the preceding gear and the following gear do not come into contact with each other, the one or more teeth being provided at a portion of the gear relating to a cut off operation

performed by the preceding and following knives in cooperation with each other.

5 A cut off apparatus as set forth in claim 12 is characterized in that, in the apparatus as set forth in claim 10, ~~a part of at least either one of the preceding~~ gear and the following gear has no teeth so that the preceding gear and the following gear do not come into contact with each other, the part with no teeth being provided at a portion of the gear relating to a cut off operation performed by the preceding and following knives
10 in cooperation with each other.

[0012]

A cut off apparatus as set forth in claim 13 is characterized in that, in the apparatus as set forth in
15 claim 10, wherein at least either one of the preceding gear and the following gear has one or more teeth shaped so that the preceding gear and the following gear do not come into contact with each other after passing a specified distance from initiation of a cut off operation, the one
20 or more teeth being provided at a portion of the gear relating to the cut off operation performed by the preceding and following knives in cooperation with each other.

[0013]

A cut off apparatus as set forth in claim 14 is
25 characterized in that, in the apparatus as set forth in claim 10, a part of at least either one of the preceding gear and the following gear has no teeth so that the

preceding gear and the following gear do not come into contact with each other after passing a specified distance from initiation of a cut off operation, the part without teeth being provided at a portion of the gear relating to the cut off operation performed by the preceding and following knives in cooperation with each other.

[0014]

A cut off apparatus as set forth in claim 15 is characterized in that, in the apparatus as set forth in any one of claim 10 through claim 14, the preceding and following knife cylinders are cylindrical members made of carbon fiber reinforced plastic.

A cut off apparatus as set forth in claim 16 is characterized in that the apparatus as set forth in any one of claim 10 through claim 15 comprises the cut off control apparatus as set forth in any one of claim 3 through claim 9.

[0015]

A cut off apparatus for cutting off band-like paper as set forth in claim 17 is characterized in that the apparatus comprises: a preceding knife cylinder on whose peripheral surface a preceding helical knife is provided; a following knife cylinder on whose peripheral surface a following helical knife, which cuts off band-like paper in cooperation with the preceding knife, is provided; a preceding gear attached at one of the opposite ends of the rotation axis of the preceding knife cylinder; a

following gear attached at one of the opposite ends of the rotation axis of the following knife cylinder; a preceding drive gear which has a meshing engagement with the preceding gear; a following drive gear which has a meshing engagement with the following gear; a preceding knife driving motor which rotationally drives the preceding drive gear; a following knife driving motor which rotationally drives the following drive gear; and a cut off control device which individually controls the preceding knife driving motor and the following knife driving motor, wherein at least either one of the preceding gear and the following gear has one or more teeth shaped so that the preceding gear and the following gear do not come into contact with each other after passing a specified distance from initiation of a cut off operation, the one or more teeth being provided at a portion of the gear relating to the cut off operation performed by the preceding and following knives in cooperation with each other.

[0016]

20 A cut off apparatus for cutting off band-like paper as set forth in claim 18 is characterized in that the apparatus comprises: a preceding knife cylinder on whose peripheral surface a preceding helical knife is provided; a following knife cylinder on whose peripheral surface a following helical knife, which cuts off band-like paper in cooperation with the preceding knife, is provided; a preceding gear attached at one of the opposite ends of

the rotation axis of the preceding knife cylinder; a following gear attached at one of the opposite ends of the rotation axis of the following knife cylinder; a preceding drive gear which has a meshing engagement with the preceding gear; a following drive gear which has a meshing engagement with the following gear; a preceding knife driving motor which rotationally drives the preceding drive gear; a following knife driving motor which rotationally drives the following drive gear; and a cut off control device which individually controls the preceding knife driving motor and the following knife driving motor, wherein a part of at least either one of the preceding gear and the following gear has no teeth so that the preceding gear and the following gear do not come into contact with each other after passing a specified distance from initiation of a cut off operation, the part without teeth being provided at a portion of the gear relating to the cut off operation performed by the preceding and following knives in cooperation with each other.

20

EFFECTS OF THE PRESENT INVENTION

[0017]

The invention described in each claim exerts the following effects.

25 According to the invention as set forth in claim 1, the preceding knife driving motor and the following knife driving motor are provided with a specified amount of torque

in the direction of contact, so that band-like paper is accurately cut off. By individually applying torque, the edges of the knives are made to come into contact with each other, and the cut off operation of the band-like paper is performed by the edge of one of the knives and the edge of the other knife coming into contact with each other. As a result, in comparison with a previous case in which knife cylinders with high rigidity are used and preload is applied to the edges of the knives, the cutting load is reduced in the present invention. Further, the rigidity and GD^2 of the knife cylinders are reduced, so that the necessary capacity for each knife driving motor is considerably reduced. Furthermore, the band-like paper is cut under a condition where the edge of one of the knives and the edge of the other one of the knives come into contact with each other, so that edge adjustment can be approximately (easily) performed.

[0018]

According to the present invention as set forth in claim 2, the following advantageous effects are guaranteed in addition to the effects realized by the invention as set forth in claim 1. Torque applied by the preceding knife driving motor and the following knife driving motor is cancelled, while band-like paper is being cut. Thus, paper feeding of the band-like paper is not influenced, so that it is possible to cut off the band-like paper with the utmost of accuracy.

According to the invention as set forth in claim 3,
the to-be-given torque pattern generator distributes
cutting torque necessary for cutting off the band-like
paper, thereby controlling the preceding knife driving
5 motor or the following knife driving motor. Thus, paper
feeding of the band-like paper is not influenced, so that
it is possible to cut off the band-like paper accurately.
[0019]

According to the invention as set forth in claim 4,
10 the following advantageous effects are guaranteed in
addition to the effects realized by the invention as set
forth in claim 3. The cutting torque can be changed in
accordance with the basis weight and the paper feeding
speed of the band-like paper.

15 According to the invention as set forth in claim 5,
the following advantageous effects are guaranteed in
addition to the effects realized by the invention as set
forth in claim 3 or claim 4, since a contact force is
generated between the preceding knife and the following
20 knife while the band-like paper is being cut, it is possible
to suppress an edge gap between the preceding knife and
the following knife.
[0020]

According to the invention as set forth in claim 6,
25 the following advantageous effects are guaranteed in
addition to the effects realized by any one of claim 3
through claim 5. It is possible to select an appropriate

to-be-given torque pattern in accordance with the paper feeding speed.

According to the invention as set forth in claim 7, the following advantageous effects are guaranteed in addition to the effects realized by any one of claim 3 through claim 6. It is possible to realize the optimum cutting of the band-like paper in accordance with the paper feeding speed, by using an even torque pattern when the rotation speed of the preceding knife driving motor and the following knife driving motor is low or intermediate, and by using a rectangular-shaped torque pattern when the rotation speed of the two knife driving motors is high.

[0021]

According to the invention as set forth in claim 8, the following advantageous effects are guaranteed in addition to the effects realized by any one of claim 3 through claim 7. Since the same torque pattern is given to the preceding knife driving motor and the following knife driving motor, the paper feeding of the band-like paper is not influenced while the band-like paper is being cut, so that the band-like paper can be cut off accurately.

According to the invention as set forth in claim 9, the following advantageous effects are guaranteed in addition to the effects realized by any one of claim 3 through claim 8. It is possible for the production management device to change the basis weight of the band-like paper to be cut off and the sheet length to be

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cut off. Further, in comparison with the previous art, in which the cutting load corresponding to the maximum basis weight is always applied, it is possible, in the present invention, to change the cutting load in accordance with the basis weight of the band-like paper, so that the wearing away of each knife is reduced, thereby lengthening the life of each knife.

[0022]

According to the invention as set forth in claim 10, since the rated capacities of the preceding knife driving motor and the following knife driving motor are the same, it is possible to employ the driving motors with the same capacity and also the power amplifiers with the same capacity.

According to the present invention as set forth in claim 11 and claim 12, the following advantageous effects are guaranteed in addition to the effects realized by the invention as set forth in claim 10. When the preceding knife and the following knife are not in contact with each other, the preceding gear and the following gear have a meshing engagement with each other while the preceding knife driving motor and the following knife driving motor are operated in synchronism with each other, or are operated in acceleration or deceleration, so that synchronism is reliably guaranteed. In addition, when the two knives are in contact with each other while cutting the band-like paper, the preceding gear and the following gear do not

have a meshing engagement, so that it is possible to control the preceding knife driving motor and the following knife driving motor separately. This realizes an appropriate cutting force.

5 [0023]

According to the present invention as set forth in claim 13 and claim 14, correct knife order can be maintained, and it can be prevented that the following knife precedes the preceding knife (inverse edge) at the initiation of the cutting operation between the preceding knife and the following knife. This will prevent damage to both knives, so that a high-quality and accurate cutting operation is possible.

According to the invention as set forth in claim 15, the following advantageous effects are guaranteed in addition to the effects realized by the invention as set forth in any one of claim 10 through claim 14. It is possible to reduce the rotational inertial force of the preceding knife cylinder and the following knife cylinder, so that control without delay is available.

[0024]

According to the invention as set forth in claim 16, the effect as set forth any of claim 3 through claim 9 in addition to any one of claim 10 through claim 15 is realized.

According to the invention as set forth in claim 16 and claim 17, it can be prevented that the following

knife precedes the preceding knife (inverse edge) at the initiation of the cutting operation between the preceding knife and the following knife. This will prevent damage to both knives, so that a high-quality and accurate cutting operation is possible.

BRIEF DESCRIPTION OF THE DRAWINGS

[0025]

[FIG. 1] FIG. 1 is a schematic front view of a cut off apparatus according to one preferred embodiment of the present invention;

[FIG. 2] FIG. 2 is a section taken along the arrow line A-A of FIG. 1;

[FIG. 3] FIG. 3 is a schematic side view showing the state of the upper and the lower gear at the time the upper and lower knives of the cut off apparatus of the present embodiment start a cut off operation;

[FIG. 4] FIG. 4 is a schematic side view showing the state of the upper and the lower gear at the time the upper and lower knives of the cut off apparatus of the present embodiment complete the cut off operation;

[FIG. 5] FIG. 5 is a control block diagram showing a cut off control device according to the present embodiment;

[FIG. 6] FIG. 6(A) through FIG. 6(E) are diagrams each showing a control pattern for each knife driving motor according to the present embodiment;

[FIG. 7] FIG. 7 is a diagram showing another example of a torque pattern given by each knife driving motor according to the present invention; and

[FIG.8] FIG. 8 is a schematic front view showing a
5 previous cut off apparatus.

REFERENCES

[0026]

- 1...frame
- 10 2...upper (preceding) knife cylinder
- 3...lower (following) knife cylinder
- 4...upper (preceding) knife
- 5...lower (following) knife
- 6,7...rotation axis
- 15 8...upper (preceding) gear
- 8a,8b...split gear
- 9...lower (following) gear
- 10...upper (preceding) drive gear
- 11...lower (following) drive gear
- 20 12...upper (preceding) knife driving motor
- 13...lower (following) knife driving motor
- 14...encoder
- 20...cut off control device
- 21...instruction value computing unit
- 25 22...position computing unit
- 23...cutting torque computing unit
- 24...speed pattern generator

	25...to-be-given torque pattern generator
	30...upper (preceding) knife speed control unit
	31...comparator
	32...instruction torque computing unit
5	33...instruction torque subtractor
	34...upper (preceding) power amplifier
	35...lower (following) knife speed control unit
	36...instruction torque adder
	37...lower (following) power amplifier
10	40...production management device
	41...paper feed control device
	D...band-like paper
	C...start point of a cut off operation
	O...end point of a cut off operation
15	S...leading ends of the upper and lower knives (start point of contact)
	E...terminal ends of the upper and lower knives (end point of contact)
	t1...time when contact starts
20	t2...time at start of speed reduction
	t3...time when waiting is started
	t4...time when 1 cycle is completed
	tc...time at start of cut-off operation
	to...time at end of cut-off operation
25	Vs...paper feeding speed
	L...sheet length to be cut off
	W...basis weight

B...width of the band-like paper

Pt...current position

Tt...rotational torque instruction value

Vt...speed instruction value

5 Txa,Txb...cutting torque

Txat,Txbt...to-be-given torque instruction value

St...detected speed

Q...specified length

10 BEST MODE FOR CARRYING OUT THE INVENTION

[0027]

A description will be made hereinbelow of a best mode for carrying out the invention. FIG. 1 is a schematic front view of a cut off apparatus according to one preferred
15 embodiment of the present invention; FIG. 2 is a section taken along the arrow line A-A of FIG. 1; FIG. 3 is a schematic side view showing the state of the upper and the lower gear at the time the upper and lower knives of the cut off apparatus of the present embodiment start a cut off
20 operation; FIG. 4 is a schematic side view showing the state of the upper and the lower gear at the time the upper and lower knives of the cut off apparatus of the present embodiment complete the cut off operation; FIG. 5 is a control block diagram showing a cut off control device
25 according to the present embodiment; FIG. 6(A) through FIG. 6(E) are diagrams each showing a control pattern for each knife driving motor according to the present

embodiment; FIG. 7 is a diagram showing another example of a pressure torque (to-be-given torque) pattern given by each knife driving motor according to the present invention.

5 [0028]

First of all, referring to FIG. 1 and FIG. 2, a description will be made of a construction of a cut off apparatus for cutting off band-like paper *D* such as a corrugated fiberboard web in a corrugating machine. As shown in FIG. 1 and FIG. 2, parallel rotational axes 6 and 7 are provided, passing through the frames 1 and 1 on both sides. Here, the rotational axes 6 and 7 are made of metal and have high rigidity.

[0029]

15 On the peripheral surfaces of the rotational axes 6 and 7, an upper (preceding) knife cylinder 2 and a lower (following) knife cylinder 3, which have cylindrical shapes, are attached via radial posts. The upper knife cylinder 2 and the lower knife cylinder 3 are made of a material, for example, CFRP (Carbon Fiber Reinforced Plastic: called carbon fiber for short), with high rigidity but with small GD^2 (rotational inertial force). Such shapes and materials of the rotational axes 6 and 7 and the upper and lower knife cylinders 2 and 3 reduce GD^2 ,
20 thereby making it possible to realize rotation control superior in responsibility and rapidity.

[0030]

In the previous art, the upper and lower knife cylinders 2 and 3 are made of a material with large GD^2 , and preload generated by the rotational inertial force and by a bend of one of the upper and lower knives provides
5 a pressing force necessary for cutting off the band-like paper *D*. As will be described below, however, torque given by the upper (preceding) knife driving motor 12 and the lower (following) knife driving motor 13 provides a cutting force in the present embodiment, so that the upper knife
10 cylinder 2 and the lower knife cylinder 3 can be made of a material with small GD^2 (rotational inertial force).
[0031]

On the peripheral surface of the upper knife cylinder 2, an upper (preceding) knife 4 with a vertical edge, which
15 faces outwards in the radial direction, is attached in the helical form. On the peripheral surface of the lower knife cylinder 3, a lower (following) knife 5 with a horizontal edge, which extends in the peripheral direction, is attached in helical form. When cutting band-like paper
20 *D*, such as a corrugated fiberboard web, the upper knife 4 and the lower knife 5 operate in cooperation. More specifically, the band-like paper is sandwiched between the upper knife 4 and the lower knife 5, which are pressed against each other. The point at which the edges of the
25 two knives come into contact with each other moves from one of the ends of the band-like paper to the other end
thereof, whereby the band-like paper is cut off. Here,

in FIG. 1 and FIG. 2, reference character *S* designates the leading end (the cutting start point) of the upper and lower knives, and reference character *E* designates the terminal end (the cutting end point) of the upper and lower knives.

[0032]

The previous art employs a knife cylinder with high rigidity to apply preload to the edge of the knife for a cutting operation. As described so far, however, according to the present embodiment, the upper knife 4 and the lower knife 5 engage in the direction in which the edge of the upper knife 4 and the edge of the lower knife 5 come into contact with each other, whereby the band-like paper *D* is cut, so that the preload is considerably reduced and adjustment of the edges of the knives can be roughly (easily) performed. Further, as will be described below, as torque is given to each of the cylinders, the rigidity of each knife cylinder 2 and 3 and their GD^2 are reduced. In addition, in contrast to the previous art in which cutting load corresponding to the maximum basis weight is always applied, the present art is capable of changing the cutting load (torque) depending upon the basis weight of the band-like paper *D*, so that the life-time of each knife 4 and 5 is increased.

[0033]

Here, FIG. 2 exaggerates the upper knife 4 and the lower knife 5 for purposes of illustration, and in an actual

case, the diameters of the upper knife cylinder 2 and the lower knife cylinder 3 are significantly large. A helical recess is provided on a part of each knife cylinder 2 and 3, and the upper knife 4 and the lower knife 5 are fitted
5 into the recesses.

Further, the upper knife 4, the lower knife 5, the upper knife cylinder 2, the lower knife cylinder 3, the rotational axes 6 and 7 can be constructed in the following way. That is, each of the upper knife cylinder 2 and the
10 lower knife cylinder 3 is a hollow cylindrical member made of carbon fiber reinforced plastic with disk-like lids at the opposite ends thereof (or formed in one piece). At the centers of the lids, rotational axes 6 and 7 made of metal are bonded or fixed with bolts and nuts, etc.
15 On the peripheral surface of the upper knife cylinder 2 and the lower knife cylinder 3, which have cylindrical shapes made of carbon fiber reinforced plastic, holders made of aluminum or iron or carbon fiber reinforced plastic are attached. On each of the holders, the upper knife 4
20 and the lower knife 5 are mounted respectively in helical form with bolts and nuts, etc. Further, at the opposite ends of the upper knife cylinder 2 and the lower knife cylinder 3 with a hollow cylindrical shape made of carbon fiber reinforced plastic, rotational axes 6 and 7 with
25 metal lids can be fixed.

[0034]

On one end-(the right-part of FIG. 1) of the rotational

axis 6, an upper (preceding) gear 8 including split gears 8a and 8b is attached. On one end (the right part of FIG. 1) of the rotational axis 7, the lower (following) gear 9 which has a meshing engagement with the upper gear 8 is attached. Two split-gears 8a and 8b are fixed to the rotational axis 6 slightly shifted from each other in the rotational direction, so that backlash in meshing engagement with the lower gear 9 while the upper knife 4 and the lower knife 5 are not in contact with each other is prevented. In this instance, the upper gear 8 can be formed as a single gear and the lower gear 9 can be formed by two split gears. Further, the upper gear 8 or the lower gear 9 is not necessarily formed by two gears, and each of the upper gear 8 and the lower gear 9 can be prepared as a single gear.

[0035]

An upper (preceding) knife driving motor 12 is connected to the upper gear 8 via an upper (preceding) drive gear 10, which has a meshing engagement with the upper gear 8. A lower (following) knife driving motor 13 is connected to the lower gear 9 via a lower (following) drive gear 11 which has a meshing engagement with the lower gear 9. These knife driving motors 12 and 13 are torque motors with the same rated capacity and the same output power, and these motors 12 and 13 are individually controlled by a cut off control device 20. Either one (for example, the lower knife driving motor 13) of these motors

12 and 13 is attached with an encoder 14 which detects the rotational speed of the motor.

[0036]

The upper gear 8 and the lower gear 9 have the following
5 characteristic features. The upper gear 8 and the lower
gear 9 have a meshing engagement with each other without
backlash in a range thereof in which the upper knife 4
and the lower knife 5 do not come into contact with each
other. As shown in FIG. 3 and FIG. 4, in a range (from
10 the cutting start point C to the cutting end point O) in
which the upper knife 4 and the lower knife 5 come into
contact with each other, thereby carrying out a cutting
operation, one of the opposite sides of the teeth of at
least one of the split gears 8a and 8b, which side faces
15 the teeth of the lower gear 9 when pressure (given) torque
 T_{xat} and T_{xbt} is applied, is cut as shown with shaded areas
in FIG. 3 and FIG. 4. In this manner, at least in a range
from the cutting start point C to the cutting end point
O, the edges of the upper knife 4 and the lower knife 5
20 come into contact with each other, but the teeth of the
upper gear 8 and the lower gear 9 do not come into contact
with each other.

[0037]

Here, the cutting start point C and the cutting end
25 point O depend on the width B of the band-like paper D.

Accordingly, in a range from the leading end (cutting start
—point)—S of the upper and lower knives to the terminal

end (cutting end point) *E* of the upper and lower knives, shaded areas in FIG. 3 and FIG. 4 are cut.

With this arrangement, it becomes possible for the upper knife driving motor 12 and the lower knife driving motor 13 to operate in synchronization with each other with reliability when the upper knife 4 and the lower knife 5 do not come into contact with each other. Further, when the upper knife 4 and the lower knife 5 come into contact with each other, thereby carrying out a cutting operation (or when the upper knife 4 and lower knife 5 are in contact with each other), the upper gear 8 and the lower gear 9 do not have a mesh engagement with each other. Thus, the upper knife driving motor 12 and the lower knife driving motor 13 can be controlled separately, thereby providing an appropriate pressing force between the upper knife 4 and the lower knife 5, so that an optimum cutting force is realized for the band-like paper *D*.

[0038]

Here, if each of the upper gear 8 and lower gear 9 is provided as a single gear, one of the opposite sides of the teeth of at least one of the upper gear 8 and the lower gear 9, which teeth are arranged in a range from the cutting start point *C* to the cutting end point *O* [or a range from the leading end (cutting start point) *S* to the terminal end (cutting end point) *E* of the upper and lower knives], should be cut. Further, at least either one of the upper gear 8 and the lower gear 9 can be formed

so as not to have any teeth in a range from the cutting start point *C* to the cutting end point *O*. Furthermore, the width of all the teeth of either one of the upper gear 8 and the lower gear 9 can be reduced.

5 [0039]

Here, if the teeth of the upper gear 8 and the lower gear 9 in a range from the leading end *S* of the upper and lower knives to the terminal end *E* of the upper and lower knives are cut (or removed) (that is, backlash is provided for the upper gear 8 and the lower gear 9 in a range from the leading end *S* of the upper and lower knives to the terminal end *E* of the upper and lower knives), there is a possibility that the lower (following) knife 5 precedes the upper (preceding) knife 4 (that is, "inverse edge" occurs). In particular, when the timing with which torque control is started is incorrect, inverse edge often occurs.

[0040]

Therefore, to prevent the occurrence of the inverse edge, the teeth of the upper gear 8 and the lower gear 9 in a range (specified distance) corresponding to a specified length (the lengths of the edges of the upper and lower knives in the axial direction) *Q* from the leading end *S* of the upper and lower knives should not be cut (or removed). That is, backlash is not provided for the upper gear 8 and the lower gear 9 in a range corresponding to the specified length *Q* from the leading end *S* of the upper and lower knives. In addition, backlash is provided in

a range from the point after passing the specified length to the terminal end *E* of the upper and lower knives.

[0041]

5 As a result, the occurrence of inverse edge between the upper and lower knives is prevented at initiation of a cutting operation, so that damage to the upper and lower knives are prevented and a high-quality and accurate cutting operation can be realized.

10 In this instance, if the specified length Q is significantly shorter than about 100 mm, there is a possibility that the inverse edge prevention effect cannot be exerted. Further, if the specified length is significantly longer than 200 mm, there is a possibility that cutting effect which should be realized by torque

15 control is not exerted. Thus, the specified length Q preferably falls within a range of about 100 mm to 200 mm from the leading end of the upper and lower knives.

[0042]

20 Here, FIG. 3 and FIG. 4 are schematic views, in which the upper knife 4 and the lower knife 5 are separated from each other. In a practical case, however, the upper knife 4 and the lower knife 5 are provided in the vicinity of the teeth of the upper gear 8 and the lower gear 9 as shown in FIG. 2, and the edges of the upper knife 4 and the lower

25 knife 5 are arranged so as to come into contact with each other.

Further, the cut off apparatus shown in FIG. 1 and

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FIG. 2 has the upper knife 4 with a vertical edge and the lower knife 5 with a horizontal edge. The present invention, however, should by no means be limited to this, and the vertical and horizontal edges can be exchanged.

5 Further, both of the knives can have vertical edges or horizontal edges.

[0043]

Next, referring to FIG. 5, FIG. 6(A) through FIG. 6(E), and FIG. 7, a description will be made of a cut off
10 control device 20 which cuts off band-like paper, such as a corrugated fiberboard web, in a corrugating machine which manufactures corrugated fiberboard sheets or the like according to the present embodiment. The corrugating machine which manufactures corrugated fiberboard sheets,
15 etc. has a production management device 40 that manages and controls the production of the whole corrugating machine.

[0044]

The production management device 40 includes: a
20 keyboard (input unit) for inputting therethrough the basis weight (or material, thickness, width, etc.) of band-like paper D such as a corrugated fiberboard sheet, the length L of a sheet to be cut off, the paper feeding speed V_s (or the number of sheets to be cut off per unit time);
25 a display; a memory which records various types of data; and a Central Processing Unit (CPU). By inputting the basis weight W of band-like paper D such as corrugated

fiberboard sheets to be cut off and the sheet length to be cut off, it is possible to change various setting values.

[0045]

In this instance, a non-illustrated paper feeding
5 device which feeds band-like paper *D*, such as a corrugate
fiberboard web, to the cut off apparatus is provided with
a paper feed control device 41. On the basis of paper
feeding speed V_s which is sent from the production
management device 40, the paper feed control device 41
10 controls the paper feeding speed in which the band-like
paper *D* is fed.

On the other hand, the cut off apparatus is provided
with a cut off control device 20, which includes: an
instruction value computing unit 21 for generating various
15 types of patterns; an upper (preceding) knife speed control
unit 30 for controlling drive current applied to the upper
knife driving motor 12; and a lower (following) knife speed
control unit 35 for controlling drive current applied to
the lower knife driving motor 13. The production
20 management device 40 sends the paper feeding speed V_s ,
the sheet length L to be cut off, and the basis weight
 W , to the cut off control device 20.

[0046]

The instruction value computing unit 21 includes:
25 a speed pattern generator 24 for generating speed patterns;
a to-be-given torque pattern generator 25 for generating
~~a torque pattern for cutting-off band-like paper *D*; and~~

a cutting torque computing unit 23 for computing necessary torque for a cut off operation.

5 The speed pattern generator 24 receives the paper feed speed V_s and the sheet length to be cut off for band-like paper D from the production management device 40, and generates a speed pattern shown in FIG. 6(A). That is, on the basis of the paper feeding speed V_s and the sheet length to be cut off, start time t_1 of joining between the upper knife 4 and the lower knife 5, start time t_c of a cutting operation, completion time t_o of a cutting operation, time t_2 at which joining is completed and deceleration is started, time t_3 at which deceleration is completed and standby is started, time t_4 at which one cycle is completed, are computed for one cycle. Further, 15 the speeds in a speed-up step (t_0 through t_1), a knife joining step (t_1 through t_2), a speed-down step (t_2 through t_3), a standby step (t_3 through t_4), are also computed. [0047]

20 Here, during the standby time (t_3 through t_4), the speed can be zero. Further, in cases where the paper feeding speed V_s is large and the sheet length to be cut off is long, the speed can be greater in the standby time (t_3 through t_4) than in the cutting time (time between t_c and t_o). In this manner, the speed pattern shown in 25 FIG. 6(A) is generated, and the generated speed pattern is stored in an unillustrated storage device. Further, the cutting start time t_c and the cutting completion time

to are sent to the to-be-given torque pattern generator 25.

[0048]

During a cutting operation of band-like paper *D*, the
5 position computing unit 22 receives the detection speed
 S_t detected by an encoder 14 attached to the lower knife
driving motor 13. The detection speed S_t is integrated,
whereby the current position P_t of the upper knife 4 and
the lower knife 5 and elapsed time t elapsed from the start
10 time t_0 of one cycle is calculated. Then, the speed pattern
generator 24 computes the speed instruction value V_t at
the elapsed time t based on the recorded speed pattern.
This calculated speed instruction value V_t is sent to the
comparator 31.

15 [0049]

Next, the cutting torque computing unit 23 receives
the paper feeding speed V_s and the basis weight of the
band-like paper *D* from the production management device
40, and computes cutting torque ($T_{xa} + T_{xb}$) necessary for
20 cutting the band-like paper *D* having the basis weight W
at the paper feeding speed V_s by means of the upper knife
driving motor 12 and the lower knife driving motor 13.

Here, the cutting torque ($T_{xa} + T_{xb}$) is changed with
change in the paper feeding speed V_s and in the width B
25 of the band-like paper. Further, the value of cutting
torque ($T_{xa} + T_{xb}$) should be large enough to resist a cut-off
reactive force added from the band-like paper *D* to the —

upper and lower knives 4 and 5, and also to give an appropriate contact force to the upper and lower knives 4 and 5. This contact force is preferably 100 kgf to 300 kgf in the horizontal direction.

5 [0050]

With this arrangement, when the band-like paper *D* is cut, a contact force is caused between the upper knife 4 and the lower knife 5 so that an edge gap between the upper knife 4 and the lower knife 5 is suppressed to a value equal to or smaller than a limit value which can be used in a cutting operation. The computed cutting torque ($T_{xa} + T_{xb}$) is sent to the to-be-given torque pattern generator 25.

The to-be-given torque pattern generator 25 generates a to-be-given torque pattern shown in FIG. 6(C) based on the cutting torque ($T_{xa} + T_{xb}$), necessary for a cutting operation, sent from the cutting torque computing unit 23, the cutting start time t_c , and the cutting completion time t_o , and stores the generated torque pattern in an unillustrated storage device. In the to-be-given torque pattern shown in FIG. 6(C), the cutting torque T_{xa} necessary for the upper knife driving motor 12 and the cutting torque T_{xb} necessary for the lower knife driving motor 13 have the same rectangular shape. In this instance, the above to-be-given torque pattern can have a trapezoidal shape with increase from t_1 to t_c and decrease from t_o to t_2 . Further, the cutting torques T_{xa} and T_{xb} can start

to be given before the joining start time t_1 (for example, immediately before the upper and lower knives come into contact with each other). Here, as already described, backlash is not provided for the upper gear 8 and the lower
5 gear 9 in a range corresponding to a specified length Q from the leading end S of the upper and lower knives, and backlash is provided in a range after passing the specified length Q to the terminal end E of the upper and lower knives. Further, the cutting torque T_{xa} and T_{xb} are applied before
10 the joining start time t_1 , whereby inverse edges can be reliably prevented at the initiation of a cutting operation.

[0051]

It is preferable that the cutting torque T_{xa} and the
15 cutting torque T_{xb} have the same absolute value (that is, torque pattern given to the upper knife driving motor 12 and the lower knife driving motor 13 have an identical shape and are of opposite signs). This makes it possible to accurately cut the band-like paper D , with no effect
20 on the paper feeding of the band-like paper D at the time the paper D is cut.

[0052]

However, the absolute values of torque need not always be equal, and one of the cutting torques T_{xa} and
25 T_{xb} of the upper knife driving motor 12 and the lower knife driving motor 13 can be larger within a range allowed by
the rate capacity of the upper knife driving motor 12 and

the lower knife driving motor 13. Here, the meaning of the rate capacity of each torque motor of the present embodiment includes not only a permissible successive fixed power capacity but also a permissible short time
5 overload power capacity.

[0053]

The torque pattern with a rectangular shape in FIG. 6(C) is for a case where the cutting speed (paper feeding speed V_s) is low or intermediate, and the torque is constant
10 in all the range of the speed. However, if the cutting speed is high, the torque pattern shown in FIG. 7 can be employed. If the cutting speed is high, the lower knife 5 is given a cutting torque of $1.25 \cdot T_{xa}$ (this is referred to as initial-period high cutting torque) which is 1.25
15 times as large as the torque necessary at the time T_c of initiation of a cutting operation as shown in FIG. 7. After that, the cutting torque is decreased to 0.6 times as large as the cutting torque $0.6T_{xa}$ (this is referred to as middle-period low cutting torque). Then, in the latter
20 half, the cutting torque is increased again up to about one time as large as the cutting torque T_{xa} (this is referred to as terminal-period normal cutting torque). Thus, the torque has a torque pattern with such a polygonal shape. With this torque pattern having a polygonal shape, it
25 becomes possible to realize an accurate cutting operation when the cutting speed is high. Here, FIG. 7 shows a torque pattern for the lower knife driving motor 13. The upper

knife driving motor 12 has a torque pattern which has the same shape but is inverse in sign. As a to-be-given torque pattern, other arbitrary shapes than the above rectangular shape or the above shape with projections and depressions are available.

[0054]

The initial-period high cutting torque is 1.1- to 1.5-times cutting torque ($1.1 \cdot T_{xa}$ to $1.5 \cdot T_{xa}$). The middle-period low cutting torque is 0.6-times to 0.9-times cutting torque ($0.6 \cdot T_{xa}$ to $0.9 \cdot T_{xa}$). The terminal-period normal cutting torque is 0.9-times to 1.1-times cutting torque ($0.9 \cdot T_{xa}$ to $1.1 \cdot T_{xa}$).

Then, on the basis of the stored to-be-given torque pattern, the to-be-given torque instruction values T_{xat} and T_{xbt} at the elapsed time t sent from the position computing unit 22 are calculated. The to-be-given torque instruction value T_{xbt} for the upper knife driving motor 12 is sent to a torque subtractor 33, and the to-be-given torque instruction value T_{xat} for the lower knife driving motor 13 is sent to the a torque adder 36.

[0055]

The comparator 31 receives the speed instruction value V_t sent from the speed pattern generator 24 and the detection speed S_t sent from the encoder 14 and compares these values. The speed deviation $V_t - S_t$ which is to be increased or decreased, as an operation result, is sent to an instruction torque computing unit 32.

The instruction torque computing unit 32 receives the speed $V_t - S_t$ to be increased or decreased, sent from the comparator 31, and computes a rotational torque instruction value T_t to be output to the upper knife driving motor 12 and the lower knife driving motor 13. The computed rotational torque instruction value T_t is output to the torque subtractor 33 and the torque adder 36. In this case, the output pattern of the rotational torque instruction value T_t is such as that shown in FIG. 6(C). In this manner, the comparator 31 and the instruction torque computing unit 32 perform feedback control.

[0056]

The torque subtractor 33 receives the rotational torque instruction value T_t sent from the instruction torque computing unit 32 and the to-be-given torque instruction value T_{xbt} sent from the to-be-given torque pattern generator 25, performs a subtraction therebetween, and sends the output torque instruction value $T_t - T_{xbt}$ to be output by the upper knife driving motor 12 to the upper (preceding) power amplifier 34. In this case, the output torque instruction value $T_t - T_{xbt}$ has a pattern shown in FIG. 6(E). The upper power amplifier 34 computes output current based on the output torque instruction value $T_t - T_{xbt}$ and gives the driving current to the upper knife driving motor 12.

[0057]

On the other hand, the torque adder 36 receives the

rotational torque instruction value T_t sent from the instruction torque computing unit 32 and the to-be-given torque instruction value T_{xat} sent from the to-be-given torque pattern generator 25, and performs an addition
5 therebetween, and sends the output torque instruction
value $T_t + T_{xat}$ to be output by the lower knife driving motor 13 to the lower (following) power amplifier 37. In this case, the output torque instruction value $T_t - T_{xat}$ has a pattern shown in FIG. 6(D). The lower power amplifier 37
10 computes output current based on the output torque instruction value $T_t + T_{xat}$ and gives the driving current to the lower knife driving motor 13.

[0058]

The upper (preceding) power amplifier 34 and the
15 lower (following) power amplifier 37 amplify the torque instructions and generate actual output current to each servo motor.

In this case, as shown in FIG. 6(D) and FIG. 6(E), the to-be-given torque instruction values T_{xat} and T_{xbt}
20 are smaller than torque T_a , T_b , T_c , and T_d necessary for motor acceleration or deceleration. It is unnecessary to increase the rated capacity of each motor by giving a cutting force to the upper knife driving motor 12 and the lower knife driving motor 13. In addition, the upper power
25 amplifier 34 and the lower power amplifier 37 can have the same rated capacity.

— [0059] —

In this manner, in the acceleration step (from t_0 to t_1), the deceleration step (from t_2 to t_3), and the standby step (from t_3 to t_4), the upper knife driving motor 12 and the lower knife driving motor 13 operate in
5 ~~synchronism with each other.~~ In the cutting step of the band-like paper D (from t_c to t_o) or the contact step of the knives (from t_1 to t_2), the upper knife driving motor 12, as shown in FIG. 3, applies force in the direction which makes the upper knife 4 move backward, that is, in
10 the direction which pushes the lower knife 5.

[0060]

In contrast, the lower knife driving motor 13 applies force in the direction which makes the lower knife 5 move forward, that is, in the direction which pushes the upper
15 knife 4. In this manner, by means of the upper knife driving motor 12 and the lower knife driving motor 13, torque is given to the upper knife 4 and the lower knife 5 in the direction in which these knives are pressed against each other, whereby a cutting force for cutting the band-like
20 paper D is produced.

In this case, if the to-be-given torque instruction values T_{xat} and T_{xbt} , which are given to the upper knife driving motor 12 and the lower knife driving motor 13, respectively, are the same, torque given to the upper knife
25 driving motor 12 and torque given to the lower knife driving motor 13 are cancelled. Thus, force required to increase or decrease the paper feeding speed V_s is not caused, and

hence the paper feeding speed is not influenced. As a result, only force necessary for cutting is applied, so that accurate and correct cutting of the band-like paper *D* is realized.

5 [0061]

With the above arrangement, when the bank-like paper is cut, clearance between the upper knife 4 and the lower knife 5 falls within a permissive range, and adjustment of a cutting force is facilitated, so that an accurate cutting operation is performed with high reliability. In addition, even if the upper knife cylinder 2 or the lower knife cylinder 3 is bent, the upper knife driving motor 12 and the lower knife driving motor 13 appropriately give a pressing force necessary for the cutting operation, so that the upper knife cylinder 2 and the lower knife cylinder 3 with a small rotational inertial force are realized. This makes it possible to use knife driving motors 12 and 13 and power amplifiers 34 and 37 with small capacities.

10 [0062]

20 In the above description, the cut off apparatus and the control apparatus for the same are described. However, the present invention should by no means be limited to the above embodiment, and various changes or modifications may be suggested without departing from the gist of the invention. For example, although the upper knife 4 proceeds the lower knife 5 in the above embodiment, the lower knife 5 can precede the upper knife 4.

[0063]

Further, the above position computing unit 22, cutting torque computing unit 23, speed pattern generator 24, to-be-given torque pattern generator 25, upper knife speed control unit 30, comparator 31, instruction torque computing unit 32, instruction torque subtractor 33, lower knife speed control unit 35, and instruction torque adder 36, are realized in the form of electrical circuits. However, all of these can be realized as a computer program (or sequence), and the above computing unit, generator, controller, comparator, adder, and subtractor can be realized as a sub-program (or sub-sequence).

INDUSTRIAL USABILITY

15 [0064]

Since it is possible to accurately cut off band-like paper such as a corrugated fiberboard sheet, the present invention is considerably useful.